

分布定数回路 (2) 《半無限長線路》

半無限長線路では反射波がないので、①,②より $B = 0$ として、

$$\begin{cases} \dot{V}(x) = Ae^{-\gamma x} \dots \textcircled{3} \\ \dot{i}(x) = \frac{A}{Z_0} e^{-\gamma x} \dots \textcircled{4} \end{cases}$$

③,④より $\frac{\dot{V}(x)}{\dot{i}(x)} = \frac{Ae^{-\gamma x}}{\frac{A}{Z_0} e^{-\gamma x}} = Z_0 \dots \textcircled{5}$

⑤より線路の任意の点において、入力インピーダンスは Z_0

⑥,⑦より $\dot{V}(0) = E - \frac{Z}{Z_0} \dot{V}(0) \dots \textcircled{8}$

③に $x = 0$ を代入 $\dot{V}(0) = A \dots \textcircled{9}$

⑧に⑨を代入 $A = E - \frac{Z}{Z_0} A \quad A = \frac{Z_0 E}{Z + Z_0} \dots \textcircled{10}$

③,④に⑩を代入

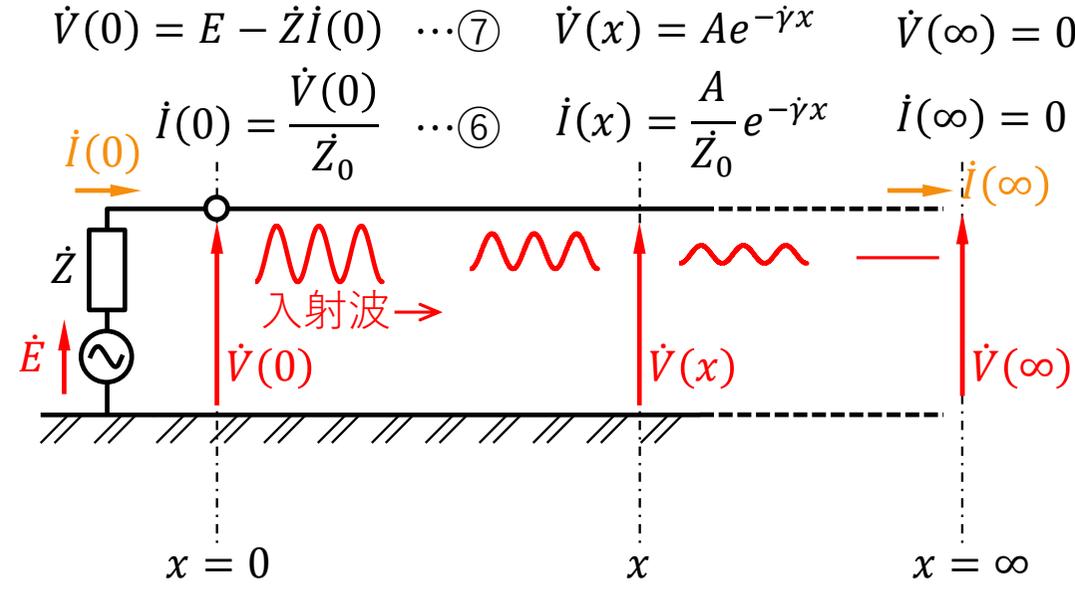
$$\begin{cases} \dot{V}(x) = \frac{Z_0 E}{Z + Z_0} e^{-\gamma x} \\ \dot{i}(x) = \frac{E}{Z + Z_0} e^{-\gamma x} \end{cases}$$

伝搬方程式の解

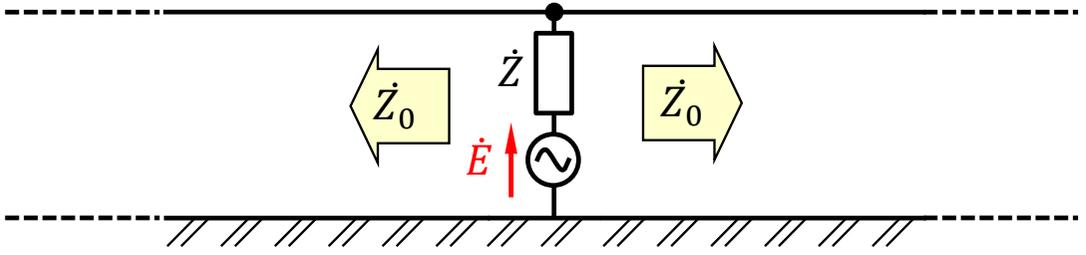
$$\begin{cases} \dot{V}(x) = \boxed{Ae^{-\gamma x}} + \boxed{Be^{\gamma x}} \dots \textcircled{1} \\ \dot{i}(x) = \frac{1}{Z_0} (Ae^{-\gamma x} - Be^{\gamma x}) \dots \textcircled{2} \end{cases}$$

伝搬定数: $\dot{\gamma} = \sqrt{(R + j\omega L)(G + j\omega C)}$

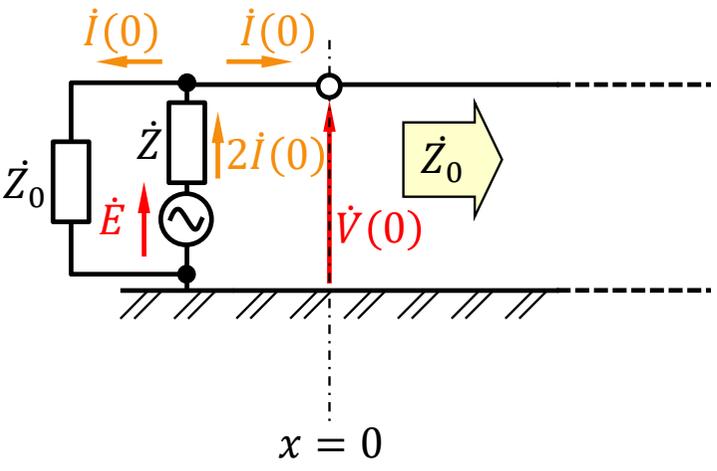
特性インピーダンス: $Z_0 = \sqrt{\frac{R + j\omega L}{G + j\omega C}}$



分布定数回路 (2) 《両無限長線路》



等価変換



$$i(0) = \frac{\dot{V}(0)}{Z_0} \dots \textcircled{3}$$

$$\dot{V}(0) = E - 2Z\dot{i}(0) \dots \textcircled{4} \quad \textcircled{1} \text{に } x=0 \text{を代入 } \dot{V}(0) = A \dots \textcircled{5}$$

$$\textcircled{4} \text{に } \textcircled{3}, \textcircled{5} \text{を代入 } A = E - \frac{2Z}{Z_0} A \quad A = \frac{Z_0 E}{2Z + Z_0} \dots \textcircled{6}$$

$$\textcircled{1}, \textcircled{2} \text{に } \textcircled{6} \text{を代入 } \begin{cases} \dot{V}(x) = \frac{Z_0 E}{2Z + Z_0} e^{-\gamma x} \\ \dot{i}(x) = \frac{E}{2Z + Z_0} e^{-\gamma x} \end{cases}$$

伝搬方程式の解

$$\begin{cases} \dot{V}(x) = \boxed{Ae^{-\gamma x}} + \boxed{Be^{\gamma x}} \dots \textcircled{1} \\ \dot{i}(x) = \frac{1}{Z_0} (Ae^{-\gamma x} - Be^{\gamma x}) \dots \textcircled{2} \end{cases}$$

伝搬定数: $\dot{\gamma} = \sqrt{(R + j\omega L)(G + j\omega C)}$

特性インピーダンス: $\dot{Z}_0 = \sqrt{\frac{R + j\omega L}{G + j\omega C}}$

分布定数回路 (2) 《有限長線路》

①,②,④より $Ae^{-\dot{\gamma}l} + Be^{\dot{\gamma}l} = \dot{Z}_l \cdot \frac{1}{\dot{Z}_0} (Ae^{-\dot{\gamma}l} - Be^{\dot{\gamma}l})$

$A(\dot{Z}_0 e^{-\dot{\gamma}l} - \dot{Z}_l e^{-\dot{\gamma}l}) + B(\dot{Z}_0 e^{\dot{\gamma}l} + \dot{Z}_l Be^{\dot{\gamma}l}) = 0$

$B = \frac{\dot{Z}_l e^{-\dot{\gamma}l} - \dot{Z}_0 e^{-\dot{\gamma}l}}{\dot{Z}_l e^{\dot{\gamma}l} + \dot{Z}_0 e^{\dot{\gamma}l}} A \quad B = \rho e^{-2\dot{\gamma}l} A \quad \left(\rho = \frac{\dot{Z}_l - \dot{Z}_0}{\dot{Z}_l + \dot{Z}_0} \right) \dots \textcircled{5}$

点lにおける反射係数は③に⑤を代入して

$\rho_l = \frac{B}{A} e^{2\dot{\gamma}l} = \frac{\rho e^{-2\dot{\gamma}l} A}{A} e^{2\dot{\gamma}l} = \rho = \frac{\dot{Z}_l - \dot{Z}_0}{\dot{Z}_l + \dot{Z}_0}$

※ $\dot{Z}_l = \dot{Z}_0$ のとき、 $\rho_l = 0$ となり、反射は生じない。

伝搬方程式の解

$\dot{V}(x) = \overset{\text{入射波}}{Ae^{-\dot{\gamma}x}} + \overset{\text{反射波}}{Be^{\dot{\gamma}x}} \dots \textcircled{1}$

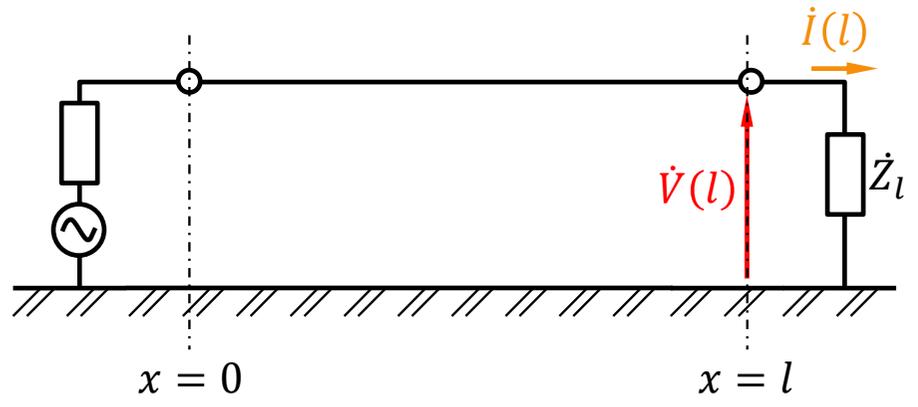
$\dot{i}(x) = \frac{1}{\dot{Z}_0} (Ae^{-\dot{\gamma}x} - Be^{\dot{\gamma}x}) \dots \textcircled{2}$

伝搬定数： $\dot{\gamma} = \sqrt{(R + j\omega L)(G + j\omega C)}$

特性インピーダンス： $\dot{Z}_0 = \sqrt{\frac{R + j\omega L}{G + j\omega C}}$

反射係数： $\rho_x = \frac{\text{反射波}}{\text{入射波}} = \frac{Be^{\dot{\gamma}x}}{Ae^{-\dot{\gamma}x}} = \frac{B}{A} e^{2\dot{\gamma}x} \dots \textcircled{3}$

$\dot{V}(l) = \dot{Z}_l \dot{i}(l) \dots \textcircled{4}$



分布定数回路 (2) 《入射波・反射波・透過波》

$$\text{反射係数} : \rho_l = \frac{Z_l - Z_0}{Z_l + Z_0} \quad \dot{V}_r = \rho_l \dot{V}_i \quad \dot{I}_r = \rho_l \dot{I}_i$$

$$\text{入射波} : \dot{I}_i = \frac{\dot{V}_i}{Z_0} \quad \text{反射波} : \dot{I}_r = \frac{\dot{V}_r}{Z_0} \quad \text{透過波} : \dot{I}_t = \frac{\dot{V}_t}{Z_l}$$

$$\begin{cases} \dot{V}_t = \dot{V}_i + \dot{V}_r & \text{電圧は入射波と同位相で反射} \\ \dot{I}_t = \dot{I}_i - \dot{I}_r & \text{電流は入射波の位相が反転して反射} \end{cases}$$

$$\begin{aligned} \text{電圧透過係数} : \lambda_{IV} &= \frac{\text{透過波}}{\text{入射波}} = \frac{\dot{V}_t}{\dot{V}_i} = \frac{\dot{V}_i + \dot{V}_r}{\dot{V}_i} = \frac{\dot{V}_i + \rho_l \dot{V}_i}{\dot{V}_i} = 1 + \rho_l \\ &= 1 + \frac{Z_l - Z_0}{Z_l + Z_0} = \frac{2Z_l}{Z_l + Z_0} \end{aligned}$$

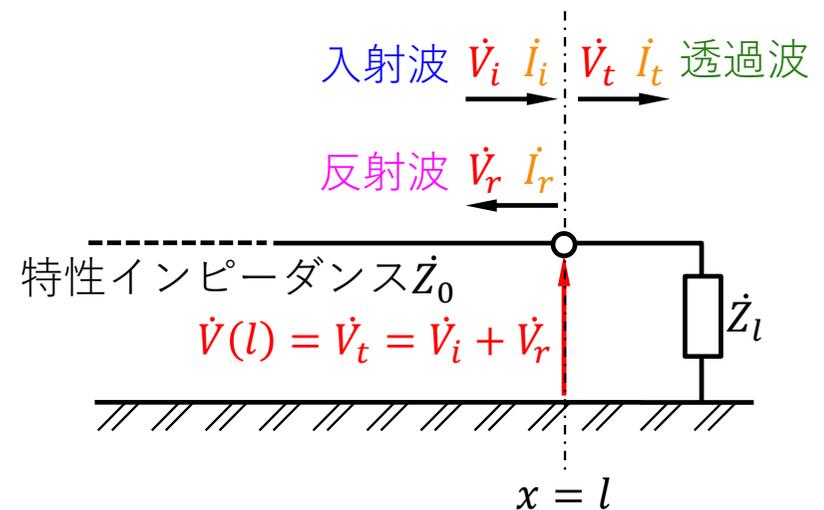
$$\begin{aligned} \text{電流透過係数} : \lambda_{II} &= \frac{\text{透過波}}{\text{入射波}} = \frac{\dot{I}_t}{\dot{I}_i} = \frac{\dot{I}_i - \dot{I}_r}{\dot{I}_i} = \frac{\dot{I}_i - \rho_l \dot{I}_i}{\dot{I}_i} = 1 - \rho_l \\ &= 1 - \frac{Z_l - Z_0}{Z_l + Z_0} = \frac{2Z_0}{Z_l + Z_0} \end{aligned}$$

伝搬方程式の解

$$\begin{cases} \dot{V}(x) = \overset{\text{入射波}}{Ae^{-\gamma x}} + \overset{\text{反射波}}{Be^{\gamma x}} \\ \dot{I}(x) = \frac{1}{Z_0} (Ae^{-\gamma x} - Be^{\gamma x}) \end{cases}$$

$$\text{伝搬定数} : \gamma = \sqrt{(R + j\omega L)(G + j\omega C)}$$

$$\text{特性インピーダンス} : Z_0 = \sqrt{\frac{R + j\omega L}{G + j\omega C}}$$



分布定数回路 (2) 《反射・透過現象》

■開放 $Z_l = \infty$

$$\rho_l = \frac{1 - \frac{Z_0}{Z_l}}{1 + \frac{Z_0}{Z_l}} = 1 \quad \lambda_{UV} = 2 \quad \lambda_{UI} = 0$$

$$\begin{aligned} \dot{V}_t &= \dot{V}_i + \dot{V}_r = 2\dot{V}_i = \lambda_{UV}\dot{V}_i & \times \dot{V}_r &= \rho_l \dot{V}_i = \dot{V}_i \\ \dot{I}_t &= \dot{I}_i - \dot{I}_r = 0 = \lambda_{UI}\dot{I}_i & \times \dot{I}_r &= \rho_l \dot{I}_i = \dot{I}_i \end{aligned}$$

■短絡 $Z_l = 0$

$$\rho_l = \frac{Z_l - Z_0}{Z_l + Z_0} = -1 \quad \lambda_{UV} = 0 \quad \lambda_{UI} = 2$$

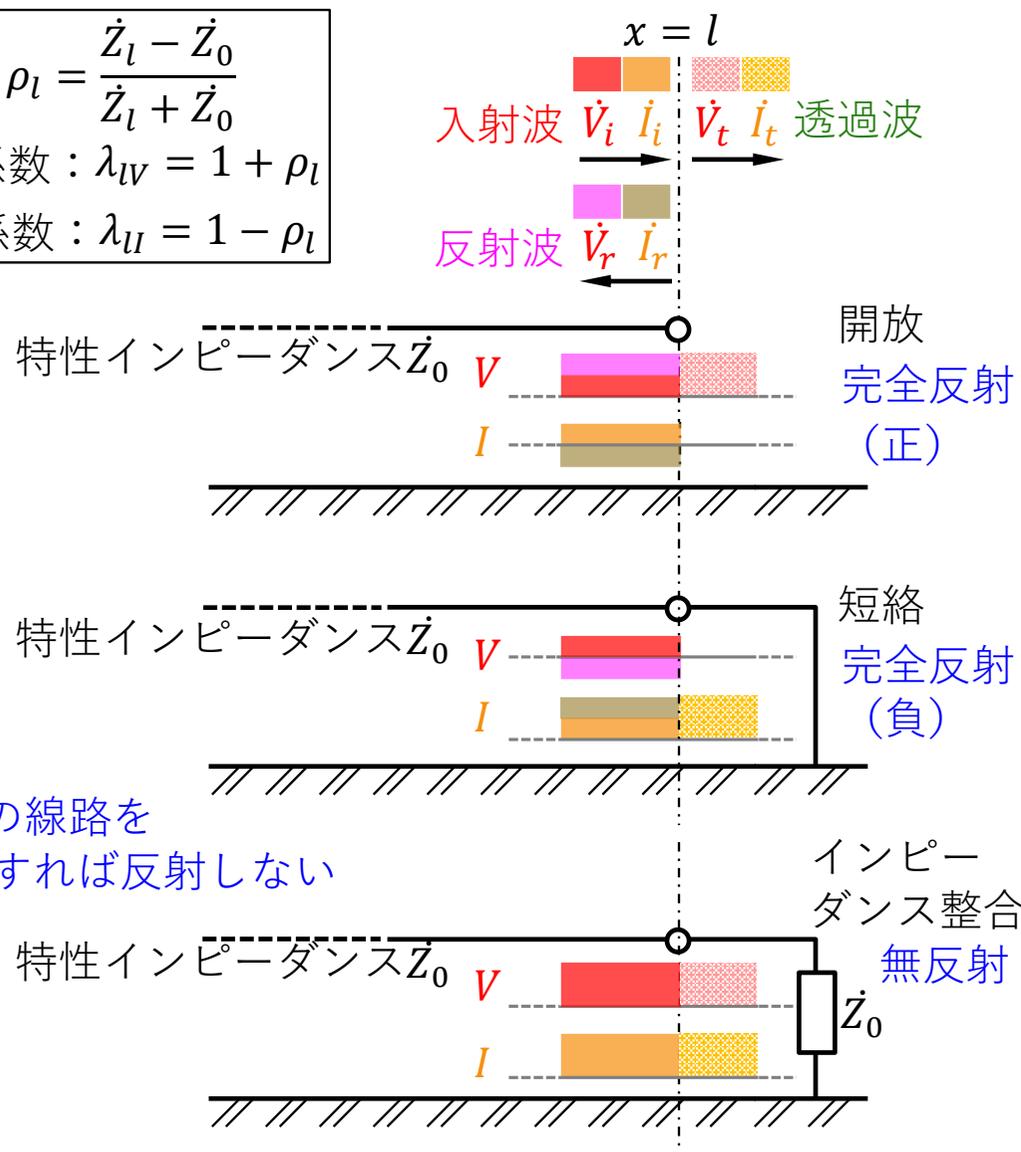
$$\begin{aligned} \dot{V}_t &= \dot{V}_i + \dot{V}_r = 0 = \lambda_{UV}\dot{V}_i & \times \dot{V}_r &= \rho_l \dot{V}_i = -\dot{V}_i \\ \dot{I}_t &= \dot{I}_i - \dot{I}_r = 2\dot{I}_i = \lambda_{UI}\dot{I}_i & \times \dot{I}_r &= \rho_l \dot{I}_i = -\dot{I}_i \end{aligned}$$

■インピーダンス整合 $Z_l = Z_0$ ※特性インピーダンス Z_0 の線路を
 $Z_l = Z_0$ なる負荷で終端すれば反射しない

$$\rho_l = \frac{Z_l - Z_0}{Z_l + Z_0} = 0 \quad \lambda_{UV} = 1 \quad \lambda_{UI} = 1$$

$$\begin{aligned} \dot{V}_t &= \dot{V}_i + \dot{V}_r = \dot{V}_i = \lambda_{UV}\dot{V}_i & \times \dot{V}_r &= \rho_l \dot{V}_i = 0 \\ \dot{I}_t &= \dot{I}_i - \dot{I}_r = \dot{I}_i = \lambda_{UI}\dot{I}_i & \times \dot{I}_r &= \rho_l \dot{I}_i = 0 \end{aligned}$$

$$\begin{aligned} \text{反射係数} : \rho_l &= \frac{Z_l - Z_0}{Z_l + Z_0} \\ \text{電圧透過係数} : \lambda_{UV} &= 1 + \rho_l \\ \text{電流透過係数} : \lambda_{UI} &= 1 - \rho_l \end{aligned}$$



分布定数回路 (2) 《透過波の式の導出 1》

反射係数 : $\rho_l = \frac{\dot{Z}_l - \dot{Z}_0}{\dot{Z}_l + \dot{Z}_0} \dots \textcircled{1}$ $\dot{V}_r = \rho_l \dot{V}_i \dots \textcircled{2}$ $I_r = \rho_l I_i$

入射波 : $I_i = \frac{\dot{V}_i}{\dot{Z}_0} \dots \textcircled{3}$ 反射波 : $I_r = \frac{\dot{V}_r}{\dot{Z}_0}$ 透過波 : $I_t = \frac{\dot{V}_t}{\dot{Z}_l} \dots \textcircled{4}$

$\dot{V}_t = \dot{V}_i + \dot{V}_r \dots \textcircled{5}$ $I_t = I_i - I_r$

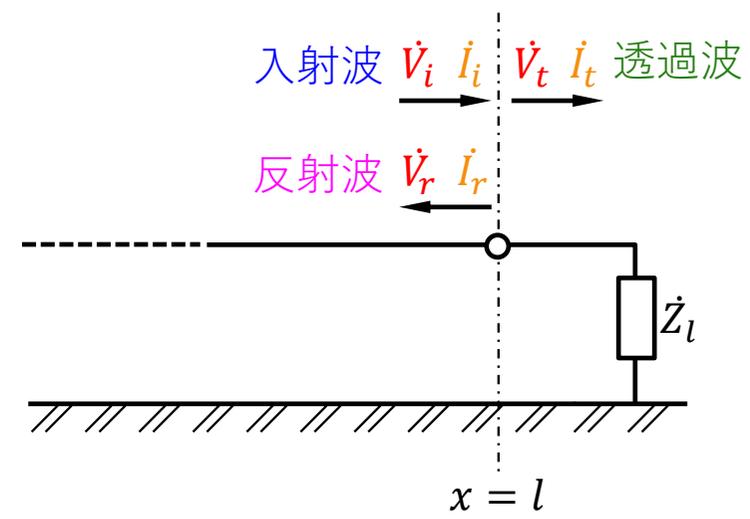
$\textcircled{1}, \textcircled{2}$ より $\dot{V}_r = \frac{\dot{Z}_l - \dot{Z}_0}{\dot{Z}_l + \dot{Z}_0} \dot{V}_i \dots \textcircled{6}$ $I_r = \frac{\dot{Z}_l - \dot{Z}_0}{\dot{Z}_l + \dot{Z}_0} I_i$

$\textcircled{5}, \textcircled{6}$ より $\dot{V}_t = \dot{V}_i + \frac{\dot{Z}_l - \dot{Z}_0}{\dot{Z}_l + \dot{Z}_0} \dot{V}_i = \frac{2\dot{Z}_l}{\dot{Z}_l + \dot{Z}_0} \dot{V}_i \dots \textcircled{7}$

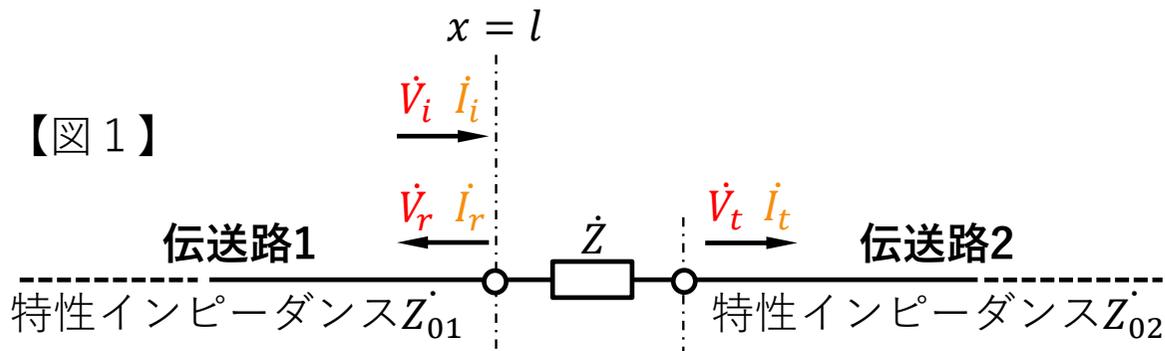
$\textcircled{3}, \textcircled{4}, \textcircled{7}$ より $I_t = \frac{\dot{V}_t}{\dot{Z}_l} = \frac{2\dot{Z}_l}{\dot{Z}_l + \dot{Z}_0} \dot{V}_i \cdot \frac{1}{\dot{Z}_l} = \frac{2}{\dot{Z}_l + \dot{Z}_0} \dot{V}_i = \frac{2\dot{Z}_0}{\dot{Z}_l + \dot{Z}_0} I_i$

電圧透過係数 : $\lambda_{UV} = 1 + \rho_l = \frac{2\dot{Z}_l}{\dot{Z}_l + \dot{Z}_0}$
 電流透過係数 : $\lambda_{UI} = 1 - \rho_l = \frac{2\dot{Z}_0}{\dot{Z}_l + \dot{Z}_0}$
 $\dot{V}_t = \lambda_{UV} \dot{V}_i$ $I_t = \lambda_{UI} I_i$

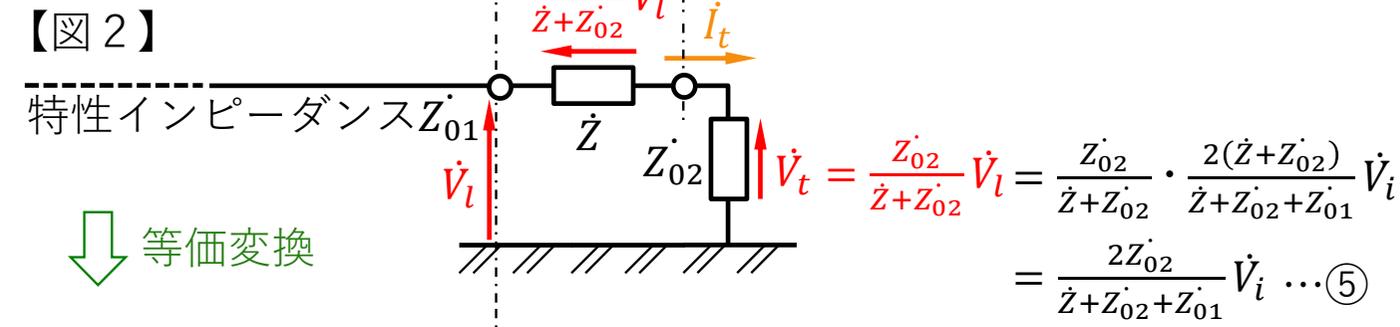
特性インピーダンス \dot{Z}_0 の伝送路



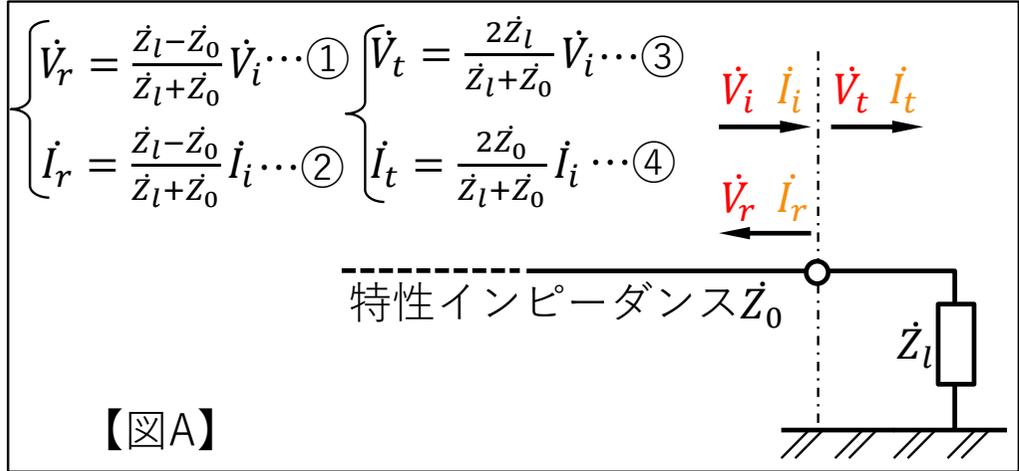
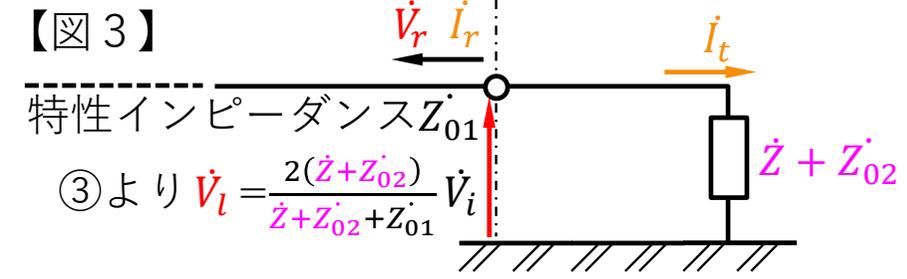
分布定数回路 (2) 《透過波の式の導出2》



↓ 等価変換



↓ 等価変換



④,⑤より

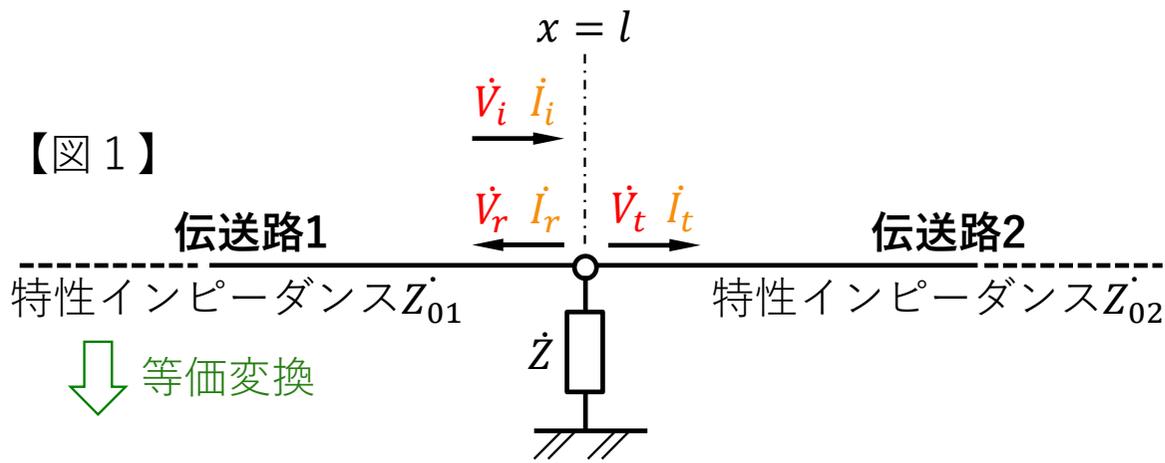
$$\begin{cases} \dot{V}_t = \frac{2Z_{02}}{Z + Z_{01} + Z_{02}} \dot{V}_i \\ \dot{I}_t = \frac{2Z_{01}}{Z + Z_{02} + Z_{01}} \dot{I}_i \end{cases}$$

①,②より

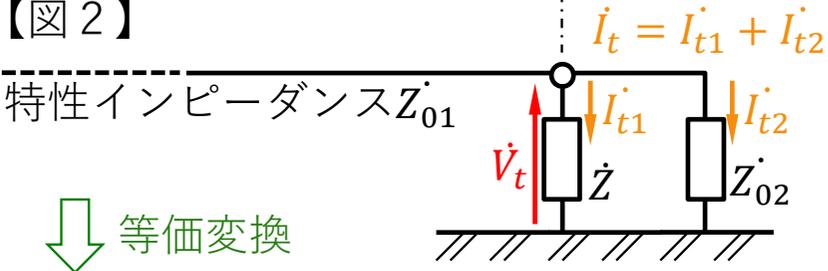
$$\begin{cases} \dot{V}_r = \frac{Z + Z_{02} - Z_0}{Z + Z_{02} + Z_0} \dot{V}_i \\ \dot{I}_r = \frac{Z + Z_{02} - Z_{01}}{Z + Z_{02} + Z_{01}} \dot{I}_i \end{cases}$$

分布定数回路 (2) 《透過波の式の導出 3》

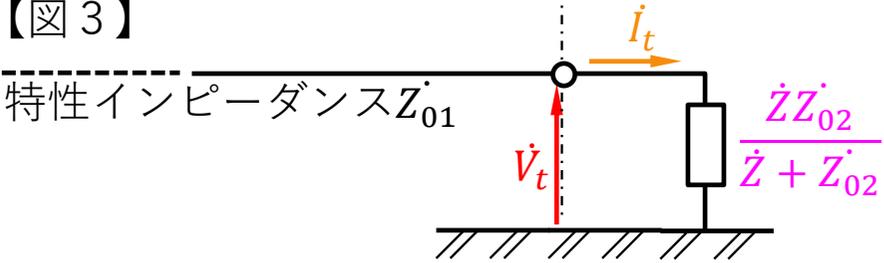
【図1】



【図2】



【図3】



$\begin{cases} \dot{V}_r = \frac{Z_l - Z_0}{Z_l + Z_0} \dot{V}_i \cdots \textcircled{1} \\ \dot{I}_r = \frac{Z_l - Z_0}{Z_l + Z_0} \dot{I}_i \cdots \textcircled{2} \end{cases}$	$\begin{cases} \dot{V}_t = \frac{2Z_l}{Z_l + Z_0} \dot{V}_i \cdots \textcircled{3} \\ \dot{I}_t = \frac{2Z_0}{Z_l + Z_0} \dot{I}_i \cdots \textcircled{4} \end{cases}$
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【図A】

③より $\dot{V}_t = \frac{2 \frac{Z Z_{02}}{Z + Z_{02}}}{\frac{Z Z_{02}}{Z + Z_{02}} + Z_{01}} \dot{V}_i = \frac{2 Z Z_{02}}{Z Z_{01} + Z Z_{02} + Z_{01} Z_{02}} \dot{V}_i$

④より $\dot{I}_t = \frac{2 Z_{01}}{\frac{Z Z_{02}}{Z + Z_{02}} + Z_{01}} \dot{I}_i = \frac{2 Z_{01} (Z + Z_{02})}{Z Z_{01} + Z Z_{02} + Z_{01} Z_{02}} \dot{I}_i$

①より $\dot{V}_r = \frac{\frac{Z Z_{02}}{Z + Z_{02}} - Z_{01}}{\frac{Z Z_{02}}{Z + Z_{02}} + Z_{01}} \dot{V}_i = \frac{Z Z_{02} - Z Z_{01} - Z_{01} Z_{02}}{Z Z_{01} + Z Z_{02} + Z_{01} Z_{02}} \dot{V}_i$

②より $\dot{I}_r = \frac{\frac{Z Z_{02}}{Z + Z_{02}} - Z_{01}}{\frac{Z Z_{02}}{Z + Z_{02}} + Z_{01}} \dot{I}_i = \frac{Z Z_{02} - Z Z_{01} - Z_{01} Z_{02}}{Z Z_{01} + Z Z_{02} + Z_{01} Z_{02}} \dot{I}_i$